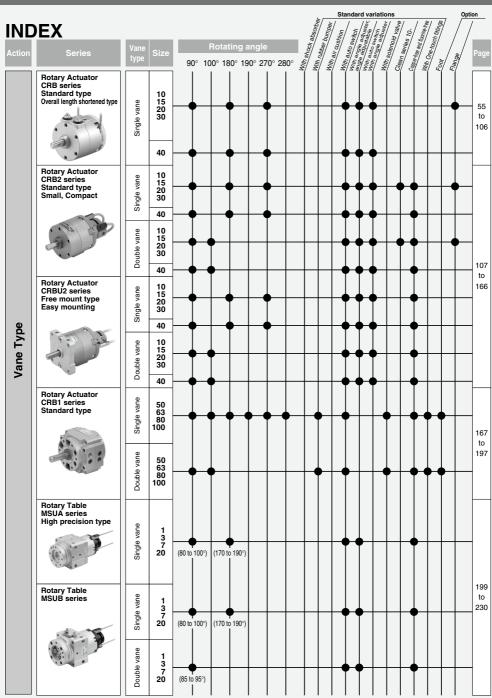


# **Series Variations**



**SMC** 

# Vane Type Rotary Actuators Series Variations

	Exterior	Eor	atures	Points of how to select	
		1 60	alui es	a rotary actuator	
	CRB, CRB2 Series Size 10, 15, 20, 30, 40	Has a compact body with exterior dimensions that do not change regard- less of the rotation angle, up to a maximum of	Round and compact type	Suitable for applications in which compactness of the actuator is particularly important.     Can be used as a part of a robot arm, due to its compact and lightweight package.  Note) There is no protrusion in the radial direction even if a switch unit or an angle adjustment unit is installed.	
Vane Type	CRBU2 Series Size 10, 15, 20, 30, 40  280°.  No backlash in terms of construction.  The piping outlets are available in two directions: the body side or the axial direction.	Can be mounted in the vertical, horizontal and axial directions.	Suitable for applications in which compactness of the actuator is important due to constraints in the mounting direction.		
Λ	CRB1 Series Size 50, 63, 80, 100	the adoption of a special seal construction.	Even if it is equipped with an auto switch, the piping outlets are available in two directions: the body side or the axial direction.	Provides a rotation angle of up to 280° and has a large torque. Suitable for appli- cations in which compact- ness of the actuator is im- portant.	
	Rotary table/High precision type MSUA Series Size 1, 3, 7, 20		Improved table top deflection 0.03 mm or less	When deflection accuracy for table top is required.	
	Rotary table MSUB Series Size 1, 3, 7, 20	Has a compact body with exterior dimensions that do not change regardless of the rotation angle, up to a maximum of 190°.      No backlash in terms of construction.	A load can be mounted directly. The rotation range can be adjusted easily. Angle adjustment is provided as standard. The body can be centered easily during installation.	Suitable for applications in which a table is required.     Suitable for applications in which compactness of the actuator is important due to constraints in the mounting direction.     Can be used as a part of a robot arm.	

# **Vane Type/Rotary Actuators Series Variations**

★ Conditions: 0.5 MPa

			D. L. P L.					* Conditions: 0.5 MPa				
	Action	Size	90°	100°	Rotatin 180°	g angle 190°		280°	★ Effective torque (N·m)	Speed regulation range (s/90°)	Allowable kinetic energy (J)	Page
		10							0.12		0.00015	
		15							0.32	0.03 to 0.5	0.0001	
	Single vane	20							0.70		0.003	
	valle	30							1.83	0.04 to 0.5	0.020	
		40							3.73	0.07 to 0.5	0.040	
		10							0.25		0.0003	
		15							0.65	0.03 to 0.3	0.0012	
	Double vane	20							1.45		0.0033	
	valle	30							3.70	0.04 to 0.3	0.020	
		40							7.59	0.07 to 0.5	0.040	
		10 0.12		0.00015	55 to 166							
		15							0.32	0.03 to 0.3	0.0001	
	Single vane	20							0.70		0.003	-
	varie	30							1.83	0.04 to 0.3	0.020	
		40							3.73	0.07 to 0.5	0.040	
		10							0.25		0.0003	
		15							0.65	0.03 to 0.3	0.0012	
	Double vane	20							1.45		0.0033	
	varie	30							3.70	0.04 to 0.3	0.020	
		40							7.59	0.07 to 0.5	0.040	
		50							5.69		0.082	
	Single	63							10.8		0.120	
	vane	80							18.0		0.398	4074-407
		100							35.9		0.600	
		50							11.8	0.1 to 1	0.112	167 to 197
	Double	63							22.7		0.160	
	vane	80							36.5		0.540	
		100							72.6		0.811	
		1							0.11		0.0065	
	Single	3							0.31		0.017	
	vane	7							0.69		0.042	
		20							1.78		0.073	
		1							0.11		0.005	
	Single	3							0.31		0.013	400.1.00
	vane	7							0.69	0.07 to 0.3	0.032	199 to 230
		20							1.78		0.056	
		1							0.23		0.005	
	Double	3							0.62		0.013	
	vane	7							1.42		0.032	
		20							3.63		0.056	1
Demontos			au au Tha		l sissan in ti	ha tabla		l della la la cala	renues entetice colum			there there

Remarks: 1. Effective torque: The values given in the table above, which are representative values, could vary according to usage conditions and thus they are not guaranteed.

2. Adjustable speed range: If the product is used below the low-speed range, it could cause the product to stick.

3. MSU series, Single vane type is angle adjustable ±5° at the edge of rotation of the angle range and ±2.5° for double vane type.

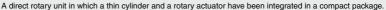
<sup>4.</sup> For the MSU series, take the moment of inertia of the table in consideration in calculating the kinetic energy of the load.



# Rack & Pinion Type Rotary Actuators Series Variations

	Exterior	Fea	atures	Points of how to select a rotary actuator		
	CRJB Series Size 05, 1 (Basic Type)	Lightweight, compact     Able to integrate the wiring and the piping in the	Can be mounted from three directions: top and bottom of the main body and the back side	Suitable for applications in which compactness of the actuator is particularly im- portant.		
	CRJU Series Size 05, 1 (With external stopper)	front side or lateral side.  No backlash.	Can be mounted from two directions: bottom of the main body and the back side Angle adjustment is possible.	Suitable for applications in which compactness of the actuator is particularly im- portant.     When angle adjustment is required.		
	CRA1 Series Size 30, 50, 63, 80, 100	Can be used at relatively slower speeds, as compared with the vane type.     Can be selected with air cushion.	A compact auto switch (D-M9 <sup>—</sup> type) can be mounted. There is a slight backlash of less than 1° due to the single piston construction. A wide variety, from small to large models, are available. These can be used with the air-hydro specifications. (Except size 30)	Suitable for applications that require a wide range of speed adjustment.     Suitable for air-hydro applications.		
Rack & Pinion Type	CRQ2 Series Size 10, 15, 20, 30, 40	(CRQ2: 10, 15 excepted)	There is no backlash be- cause the double piston type has been adopted.	Suitable for applications in which a thin profile is required.     Suitable for applications requiring no backlash.		
	Rotary table MSQ Series Size 10, 20, 30, 50 Size 1, 2, 3, 7, 10, 20, 30, 50, 70, 100, 200 Size 10, 20, 30, 50 (With external shock absorber)	A thin rotary table unit with a low table top height. No backlash. Piping direction is selectable from the edge side of the main body and the lateral side. Actuator with internal shock absorber is selectable. (Size 10, 20, 30, 50, 70, 100, 200) Actuator with external shock absorber is selectable. (Size 10, 20, 30, 50, 70, 100, 200)	The body can be centered easily during installation. A load can be mounted directly. The angle can be adjusted as desired. (Between 0° and 190°) (Adjustor bolt, Internal absorber) The body can be used as a flange.	Suitable for applications in which a table is required.     Suitable for applications in which a thin profile is required particularly.     Suitable for applications requiring no backlash.		
	3-position rotary table MSZ Series Size 10, 20, 30, 50	Can be controlled with a solenoid valve located in the 3 position pressure center. No backlash.	Right and left rotation ends can be adjustable at 0 to 95° from the central posi- tion.	Suitable for 3 position stopping.		
	Low-speed rotary actuator CRQ2X Series Size 10, 15, 20, 30, 40	Stable operation possible at 5 s/90°.	Dimensions the same as CRQ2 series.	Suitable for low-speed op-		
	Low-speed rotary table MSQX Series Size 10, 20, 30, 50		Dimensions the same as MSQ series.	eration.		

Rotary cylinder MRQ Series Size 32, 40 p. 419 to 437



- Rotation angle/80 to 100°, 170 to 190°
- Linear stroke/5, 10, 15, 20, 25, 30, 40, 50, 75, 100 mm

# Rack & Pinion Type/Rotary Actuators Series Variations

★ Conditions: 0.5 MPa

			★ Conditions: 0.5 MPa									
	A -4:	0:		Rot	tating ar	ngle		★ Effective torque	Speed regulation range	Allowable kinetic energy	D	
	Action	Size	90°	100°	180°	190°	360°	(N⋅m) .	(s/90°)	(J)	Page	
		05						0.042		0.00025		
	Single	1						0.095	0.1 to 0.5	0.001		
ra	ack pinion	05						0.042		0.0004	231 to 242	
	_	1						0.095	0.1 to 0.5	0.002		
		30						1.91	0.2 to 1	0.010		
	İ									0.050		
		50						9.27	0.2 to 2	0.98*		
	Cinala	60						17.0	0.12	1		
r	Single ack pinion -	63						17.2	0.2 to 3	1.0	243 to 292	
10	ack pillion	80						31.7	0.2 to 4	0.16		
		00						31.7	0.2 10 4	2.0*		
		100						74.3	0.2 to 5	0.54		
									0.2 10 3	2.9*		
		10						0.3	0.2 to 0.7	0.00025		
		15						0.75		0.00039		
		20						1.84		0.025	293 to 320	
	Double									0.12*		
ra	ack pinion	30		_				3.11	0.2 to 1	0.048		
	-								-	0.25 * 0.081	-	
		40						5.3		0.4*	-	
		1						0.087		0.001		
	-	2						0.18	0.2 to 0.7	0.0015		
		3						0.29		0.002		
		7						0.56	0.2 to 1	0.006	1	
		10						0.89		0.007		
		10						0.09	0.2 to 2 (Reduced height type)	0.039*		
		20						1.84	(neduced neight type)	0.025		
		20						1.01	0.2 to 1	0.116*		
	Double	30						2.73	/ With shock \	0.048	321 to 362	
ra	ack pinion								absorber:	0.116*		
		50						4.64	0.2 to 0.7	0.081		
	-								0.2 to 1.5	0.294* 0.24	-	
		70						6.79	(With shock absorber: 0.2 to 1	1.1 *		
	-								0.2 to 2	0.32		
		100						10.1	0.2 to 2 (With shock absorber: 0.2 to 1	1.6*	İ	
		200						19.8	( With shock absorber: )	0.56		
									0.2 to 1	2.9*		
		10						0.90		0.007		
	Double	20						1.78	0.2 to 1	0.025	363 to 375	
ra	ack pinion	30						2.65		0.048		
		50						4.75		0.081		
	ļ	10						0.3	0.7 to 5	0.00025		
	Double	15						0.75	0 10 0	0.00039		
	ack pinion	20						1.84	4	0.025		
[	,	30					-	3.11	1 to 5	0.048	0774	
		40 10						5.3		0.081	377 to 417	
	Double	20						0.89 1.84	-	0.007 0.025	4	
		30						2.73	1 to 5	0.025	1	
l i	ack pinion	50						4.64	1	0.048	1	
	amander: 4 5			aluga et e	in the - 4	la ab ····	ubiak		anulal van :"		hua di	
D,	omarke: 1 F	-ffective torc	up. The v	aluga giyan	in the tab	le above	which are	representative values	could vary according	to usage conditions and t	hue thou	

Remarks: 1. Effective torque: The values given in the table above, which are representative values, could vary according to usage conditions and thus they

with an air cushion.

For the MSQ series, the \* symbol indicates the value of an actuator that is equipped with a shock absorber.

4. Refer to page 355 for allowable energy of the external shock absorber type (L type, H type) for the MSQ series.



are not guaranteed.

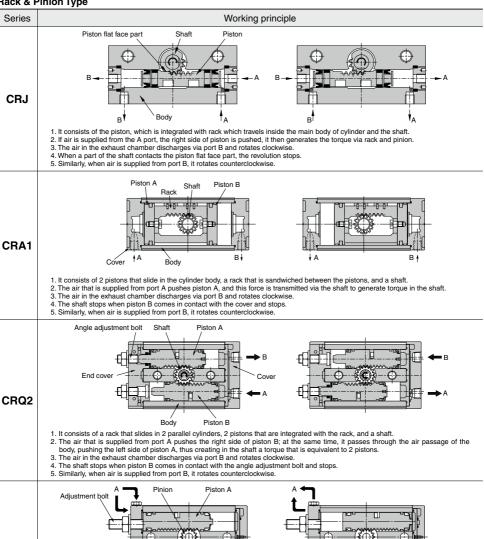
2. Adjustable speed range: If the product is used at a speed lower than the adjustment range, it may cause the product to stick or stop.

3. Allowable energy:

\* Symbol: The \* symbol in the allowable energy for the CRA1 series and the CRQ2 series indicates the value of an actuator that is equipped

# **Working Principle**

#### Rack & Pinion Type



## MSQ

- 1. It consists of a rack that slides in 2 parallel cylinders, 2 pistons that are integrated with the rack, and a pinion.
- 2. The air that is supplied from port A pushes the left side of piston A; at the same time, it passes through the air passage of the body, pushing the right side of piston B, thus creating in the shaft an amount of torque that is equivalent to 2 pistons.
- 3. The air in the exhaust chamber discharges via port B and rotates clockwise
- The pinion stops when piston B comes in contact with the adjustment bolt and stops.
- 5. Similarly, when air is supplied from port B, it rotates counterclockwise.



# Working Principle: How to Mount Loads

#### Vane Type Single vane (S) Series Double vane (D) Shaft Shaft Vane Vane Stopper Stopper CRB<sub>2</sub> CRB<sub>1</sub> Body Body CRBU2 В 1. It consists of a shaft that is integrated with the vane that 1. It consists of a shaft that is integrated with the 2 vanes that MSU slides along the inner surface of the body, and a stopper slide along the inner surface and 2 stoppers. 2. The air that is supplied from port A pushes the vane, thus 2. The air that is supplied from port A passes through the passage in the shaft in order to also supply air to the other creating torque in the shaft 3. The air in the exhaust chamber discharges via port B and chamber. Thus, the air pushes 2 vanes and creates torque

#### **How to Mount Loads**

rotates clockwise

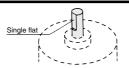
counterclockwise

#### How to connect a load directly to a single flat shaft

The vane stops as it comes in contact with the stopper.

5. Similarly, when air is supplied from port B, it rotates

To secure the load, select a bolt of an appropriate size from those listed in tables 1 and 2 by taking the shaft's single flat bearing stress strength into consideration.



#### Table (1) Directly Fixed with Bolts (Refer to Figure (1).)

Model	Size	Shaft bore size	Screw
CRQ2	10	5	M5 or larger
Chuz	15	6	IVIO OI IAIGEI
	10	4	M4 or larger
CRB2	15	5	M5 or larger
CNDZ	20	6	IVIS OF larger
	30	8	M6 or larger
	10	4	M4 or larger
CRBU2	15	5	M5 or larger
CNBUZ	20	6	IVIS OF larger
	30	8	M6 or larger
CRJ	05	5	M5 or larger
Chu	1	6	Wio or larger

#### Table (2) Fixed with a Holding Block (Refer to Figure (2).)

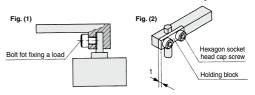
3. Its movement consists of the same rotation as that of the

in the shaft

single vane.

Model	Size	Shaft bore size	Screw	Plate thickness (t)	
CRQ2	10	5	M3 or larger	2.3 or wider	
Chuz	15	6	M4 or larger	3.6 or wider	
	10	4	M3 or larger	2 or wider	
CRB2	15	5	IVIS OF larger	2.3 or wider	
CHB2	20	6	M4 or larger	3.6 or wider	
	30	8	M5 or larger	4 or wider	
	10	4	M3 or larger	2 or wider	
CRBU2	15	5	IVIO OI IAIGEI	2.3 or wider	
CHBUZ	20	6	M4 or larger	3.6 or wider	
	30	8	M5 or larger	4 or wider	
CRJ	05	5	M3 or larger	2.3 or wider	
ChJ	1	6	M4 or larger	3.6 or wider	

The plate thickness (t) in the table above indicates a reference value when a carbon steel is used. Besides, we do not manufacture a holding block.





Calculation of Moment of Inertia	···· P.34
1-1 Equation Table of Moment of Inertia	···· P.35
1-2 Calculation Example of Moment of Inertia	···· P.36
1-3 Graph for Calculating the Moment of Inertia	···· P.38
2 Calculation of Required Torque	P.40
<b>2</b> -1 Load Type	
2-2 Effective Torque	···· P.41
2-3 Effective Torque for Each Equipment	···· P.41
<b>③</b> Confirmation of Rotation Time	···· P.43
4 Calculation of Kinetic Energy	P.44
4-1 Allowable Kinetic Energy and Rotation Time Adjustment Range	P.45
4-2 Moment of Inertia and Rotation Time	···· P.46
<b>⑤</b> Confirmation of Allowable Load	P.49
Calculation of Air Consumption and Required Air Flow Capacity	<i>J</i> P.50
<b>3</b> -1 Inner Volume and Air Consumption	···· P.51
(3-2 Air Consumption Calculation Graph	P.53

Model selection software is available.

For details, refer to the "Model Selection Software" section on the SMC website.



Refer to pages 378 to 383 for the selection of low-speed' rotary actuators CRQ2X/MSQX series.

#### **Selection Procedures**

#### Note

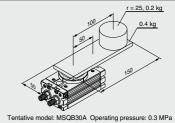
#### Selection Example

#### Operating conditions are as follows:

Operating conditions are as follows:

- Tentative models
- · Operating pressure (MPa)
- · Mounting orientation
- Load type Static load
  - Resistance load Inertial load
- · Load dimensions (m) · Load mass (kg)
- Rotation time (s) · Rotation angle (rad)

- . Refer to page 40 for the load type. . The unit for the rotation angle is radian.
  - $180^{\circ} = \pi rad$  $90^{\circ} = \pi/2 \text{rad}$



Mounting orientation: Vertical Load type: Inertial load Rotation time: t = 1.5s Rotation angle:  $\theta = \pi rad$  (180°)

#### Calculation of Moment of Inertia

Calculate the inertial moment of load. ⇒P.34

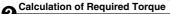
· Loads are generated from multiple parts. The inertial moment of each load is calculated, and then totaled.

Inertial moment of load 1 I<sub>1</sub> 

Inertial moment of load 2 I2  $I_2 = 0.2 \times \frac{0.025^2}{2} + 0.2 \times 0.1^2 = 0.002063$ 

Total inertial moment I

 $I = I_1 + I_2 = 0.003896 \text{ [kg-m}^2\text{]}$ 



Calculate the required torque for each load type and confirm whether the values fall in the effective torque range.

- · Static load (Ts) Required torque: T = Ts
- Resistance load (Tf)
- Required torque: T = Tf (3 to 5)
- · Inertial load (Ta)
- Required torque: T = Ta x 10 ⇒P.40

· When the resistance load is rotated, the required torque calculated from the inertial load must be added.

Required torque T = Tf x (3 to 5) + Ta x 10 Inertial load: Ta  $Ta = I \cdot \hat{\omega}$ 

 $\dot{\omega} = \frac{2\theta}{t^2} [rad/s^2]$ Required torque: T

T = Ta x 10

= 0.003896 x  $\frac{2 \times \pi}{1.5^2}$  x 10 = 0.109 [N·m]

0.109 Nm < Effective torque OK

## **Confirmation of Rotation Time**

Confirm whether the time falls in the rotation time adjustment range. ⇒P.43

. Consider the time after converted in the time per 90° (1.0 s/180° is converted in 0.5 s/90°.)

 $0.2 \le t \le 1.0$ t = 0.75s/90°OK

## Calculation of Kinetic Energy

Calculate the kinetic energy of the load and confirm whether the energy is below the allowable range. Can confirm referring to the inertial

moment and rotation time graph. (Pages 46 to 48) ⇒P.44

 If the energy exceeds the allowable range, a suitable cushioning mechanism such as a shock absorber must be externally installed.

Kinetic energy: E  $E = \frac{1}{2} I \cdot \omega^2$ 

 $\omega = \frac{2 \cdot \theta}{1}$ 

 $E = \frac{1}{2} 0.003896 \times \left(\frac{2 \times \pi}{1.5}\right)^2 = 0.03414 \text{ [J]}$ 0.03414 [J] < Allowable energy OK

#### **Confirmation of Allowable Load**

Confirm whether the load applied to the product is within the allowable range. ⇒P.49

If the load exceeds the allowable range, a bearing or similar must be externally installed

Moment load: M  $M = 0.4 \times 9.8 \times 0.05 + 0.2 \times 9.8 \times 0.1$ = 0.392 [N·m] 0.392 [N·m] < Allowable moment load OK

## Calculation of Air Consumption and Required Air Flow Capacity

Air consumption and required air flow capacity are calculated when necessary. ⇒P.50



## **1** Calculation of Moment of Inertia

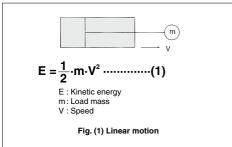
The moment of inertia is a value indicating the inertia of a rotating body, and expresses the degree to which the body is difficult to rotate. or difficult to stop.

It is necessary to know the moment of inertia of the load in order to determine the value of necessary torque or kinetic energy when selecting a rotary actuator.

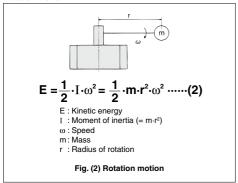
Moving the load with the actuator creates kinetic energy in the load. When stopping the moving load, it is necessary to absorb the kinetic energy of the load with a stopper or a shock absorber. The kinetic energy of the load can be calculated using the formulas shown in Figure 1 (for linear motion) and Figure 2 (for rotation motion).

In the case of the kinetic energy for linear motion, the formula (1) shows that when the velocity v is constant, it is proportional to the mass m. In the case of rotation motion, the formula (2) shows that when the angular velocity is constant, it is proportional to the moment of inertia.

#### Linear motion



#### Rotation motion

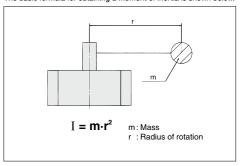


As the moment of inertia is proportional to the squares of the mass and the radius of rotation, even when the load mass is the same, the moment of inertia will be squared as the radius of rotation grows bigger. This will create greater kinetic energy, which may result in damage to the product.

When there is rotation motion, product selection should be based not on the load mass of the load, but on the moment of inertia.

#### Moment of Inertia Formula

The basic formula for obtaining a moment of inertia is shown below.



This formula represents the moment of inertia for the shaft with mass m, which is located at distance r from the shaft.

For actual loads, the values of the moment of inertia are

For actual loads, the values of the moment of inertia are calculated depending on configurations, as shown on the following page.

⇒P.35 Equation table of moment of inertia

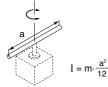
⇒P.36 and 37 Calculation example of moment of inertia ⇒P.38 and 39 Graph for calculating the moment of inertia

## 1-1 Equation Table of Moment of Inertia

I: Moment of inertia m: Load mass

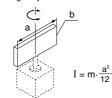
#### 1. Thin shaft

Position of rotational axis: Perpendicular to the shaft through the center of gravity



#### 2. Thin rectangular plate

Position of rotational axis: Parallel to side b and through the center of gravity



# 3. Thin rectangular plate (Including Rectangular parallelepiped)

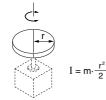
Position of rotational axis: Perpendicular to the plate through the center of gravity



$$I = m \cdot \frac{a^2 + b^2}{12}$$

#### 4. Round plate (Including column)

Position of rotational axis: Through the center axis



#### 5. Solid sphere

Position of rotational axis: Through the center of diameter



$$I = m \cdot \frac{2r^2}{5}$$

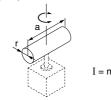
#### 6. Thin round plate

Position of rotational axis: Through the center of diameter



#### 7. Cylinder

Position of rotational axis: Through the center of diameter and gravity.



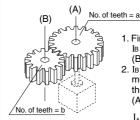
# 8. When the rotational axis and load center of gravity are not consistent



$$I = K + m \cdot L^2$$

- K: Moment of inertia around the load center of gravity
- 4. Round plate  $K = m \cdot \frac{r^2}{2}$

#### 9. Gear transmission

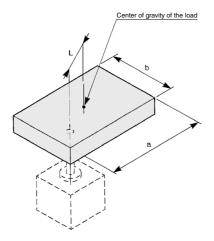


- 1. Find the moment of inertia IB for the rotation of shaft (B).
- 2. Is is converted to the moment of inertia IA for the rotation of the shaft

$$I_A = \left(\frac{a}{b}\right)^2 \cdot I_B$$

## **1**-2 Calculation Example of Moment of Inertia

#### 1 If the shaft is located at a desired point of the load:



Example: 1 If the load is the thin rectangular plate:

Obtain the center of gravity of the load as I1, a provisional shaft.

$$I_1 = m \cdot \frac{a^2 + b^2}{12}$$

② Obtain the actual moment of inertia I2 around the shaft, with the premise that the mass of the load itself is concentrated in the load's center of gravity point.

$$I_2 = m \cdot L^2$$

3 Obtain the actual moment of inertia I.

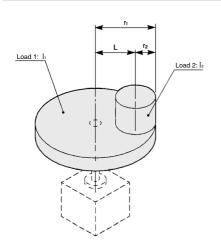
$$\begin{split} I &= I_1 + I_2 \\ \text{m: mass of the load} \\ \text{L: distance from the shaft to the load's } \\ \text{center of gravity} \end{split}$$

#### Calculation Example

$$a = 0.2 \text{ m}, b = 0.1 \text{ m}, L = 0.05 \text{ m}, m = 1.5 \text{ kg}$$

$$\begin{split} I_1 &= 1.5 \times \frac{0.2^2 + 0.1^2}{12} = 6.25 \times 10^{-3} & \text{kg·m}^2 \\ I_2 &= 1.5 \times 0.05^2 = 3.75 \times 10^{-3} & \text{kg·m}^2 \\ I &= (6.25 + 3.75) \times 10^{-3} = 0.01 & \text{kg·m}^2 \end{split}$$

## 2 If the load is divided into multiple loads:



Example: 1) If the load is divided into the 2 cylinders:

The center of gravity of load 1 matches the shaft
The center of gravity of load 2 differs from the shaft
Obtain the moment of inertia of load 1:

$$I_1 = m_1 \cdot \frac{r_1^2}{2}$$

2 Obtain the moment of inertia of load 2:

$$I_2 = m_2 \cdot \frac{r_2^2}{2} + m_2 \cdot L^2$$

3 Obtain the actual moment of inertia I:

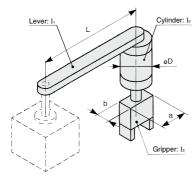
$$I = I_1 + I_2$$

#### Calculation Example

$$m_1 = 2.5 \text{ kg}, m_2 = 0.5 \text{ kg}, r_1 = 0.1 \text{ m}, r_2 = 0.02 \text{ m}, L = 0.08 \text{ m}$$

$$\begin{split} I_1 &= 2.5 \text{ x } \; \frac{0.1^2}{2} = 1.25 \text{ x } \; 10^{-2} & \text{kg} \cdot \text{m}^2 \\ I_2 &= 0.5 \text{ x } \; \frac{0.02^2}{2} + 0.5 \text{ x } 0.08^2 = 0.33 \text{ x } \; 10^{-2} & \text{kg} \cdot \text{m}^2 \\ I &= (1.25 + 0.33) \text{ x } \; 10^{-2} = 1.58 \text{ x } \; 10^{-2} & \text{kg} \cdot \text{m}^2 \end{split}$$

#### 3 If a lever is attached to the shaft and a cylinder and a gripper are mounted to the tip of the lever:



Example: 1 Obtain the lever's moment of inertia:

$$I_1 = m_1 \cdot \frac{L^2}{3}$$

② Obtain the cylinder's moment of inertia:

$$I_2 = m_2 \cdot \frac{\left(D/2\right)^2}{2} + m_2 \cdot L^2$$

3 Obtain the gripper's moment of inertia:

$$I_3 = m_3 \cdot \frac{a^2 + b^2}{12} + m_3 \cdot L^2$$

4 Obtain the actual moment of inertia:

**Calculation Example** 

 $L = 0.2 \text{ m}, \ \emptyset D = 0.06 \text{ m}, \ a = 0.06 \text{ m}, \ b = 0.03 \text{ m}, \ m_1 = 0.5 \text{ kg}, \ m_2 = 0.4 \text{ kg}, \ m_3 = 0.2 \text{ kg}$ 

$$I_1 = 0.5 \text{ x } \frac{0.2^2}{3} = 0.67 \text{ x } 10^{-2}$$

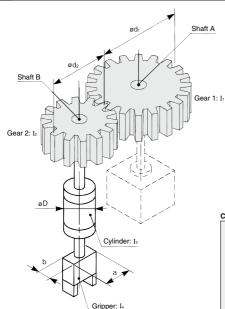
$$I_3 = 0.2 \times \frac{0.06^2 + 0.03^2}{12} + 0.2 \times 0.2^2 = 0.81 \times 10^{-2}$$

$$I_2 = 0.4 \text{ x } \frac{(0.06/2)^2}{8} + 0.4 \text{ x } 0.2^2 = 1.62 \text{ x } 10^{-2} \text{ kg·m}^2$$

 $I = (0.67 + 1.62 + 0.81) \times 10^{-2} = 3.1 \times 10^{-2}$ 

kg·m²

### 4 If a load is rotated through the gears:



Example: 1 Obtain the moment of inertia I1 around shaft A:

$$I_1 = m_1 \cdot \frac{(d_1/2)^2}{2}$$

2 Obtain moment of inertias I2, I3, and I4 around shaft B:

$$I_2 = m_2 \cdot \frac{(d_2/2)}{2}$$

$$I_4 = m_4 \cdot \frac{a^2 + b^2}{12}$$

moment of inertia IA around shaft A.  $I_A = (A/B)^2 \cdot I_B$  [A/B: ratio of the number of teeth]

4 Obtain the actual moment of inertia:

$$I = I_1 + I_A$$

/ m<sub>1</sub>: mass of gear 1 m<sub>2</sub>: mass of gear 2

m<sub>3</sub>: mass of cylinder \m₄: mass of gripper

Calculation Example

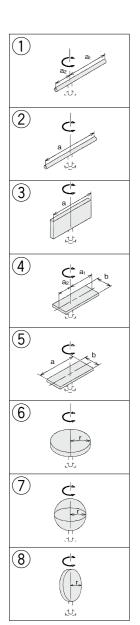
 $d_1 = 0.1 \ m, \ d_2 = 0.05 \ m, \ D = 0.04 \ m, \ a = 0.04 \ m, \ b = 0.02 \ m$ 

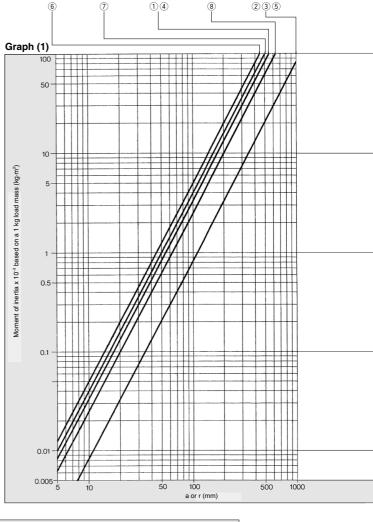
 $m_1 = 1 \text{ kg}, \ m_2 = 0.4 \text{ kg}, \ m_3 = 0.5 \text{ kg}, \ m_4 = 0.2 \text{ kg}, \ tooth \ count \ ratio = 2$  $I_{t} = 1 \quad x \quad \frac{(0.1/2)^{2}}{8} = 1.25 \, x \, 10^{-3} \, kg \cdot m^{2} \quad I_{s} = 0.2 \ x \, \frac{0.04^{2} + 0.02^{2}}{12}$ 

 $\mathrm{I_2} = 0.4 \ x \ \frac{(0.05/2)^2}{2} = 0.13 \ x \ 10^3 \ kg m^2 \\ \mathrm{I_3} = 2^2 \ x \ 0.26 \\ \mathrm{X} \ 10^3 = 1.04 \ x \ 10^3 \ kg m^2$ 

 $I_3 = 0.5 \times \frac{(0.04/2)^2}{2} = 0.1 \times 10^3 \text{ kg/m}^2$  I = (1.25 + 1.04)  $\times 10^{-3} = 2.29 \times 10^{-3} \text{ kg/m}^2$ 

## **1**-3 Graph for Calculating the Moment of Inertia



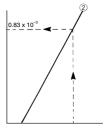


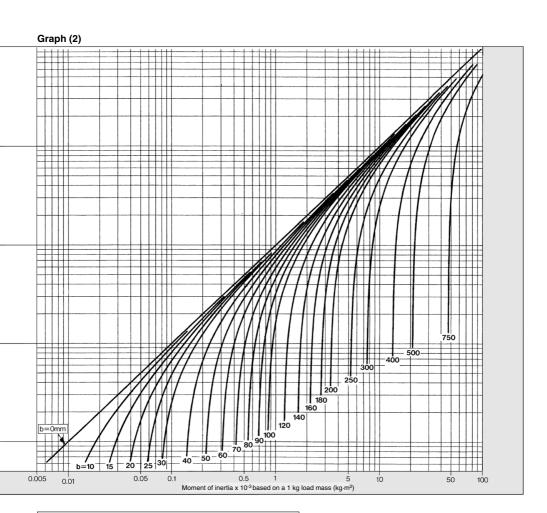
#### How to read the graph: only when the dimension of the load is "a" or "r"

[Example] When the load shape is  $\odot$ , a = 100 mm, and the load mass is 0.1 kg. In Graph (1), the point at which the vertical line of a = 100 mm and the line of the load shape  $\odot$  intersect indicates that the moment of inertia of the 1 kg mass is 0.83 x 10 $^{-1}$  kg·m<sup>2</sup>.

Because the mass of the load is 0.1~kg, the actual moment of inertia is  $0.83\times10^{-3}\times0.1=0.083\times10^{-3}~kg\cdot m^2$ .

(Note: If "a" is divided into "a¹a²", the moment of inertia can be obtained by calculating them separately.)



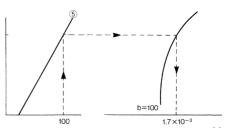


#### How to read the graph: when the dimension of the load contains both "a" and "b".

[Example] When the load shape is ⑤, a = 100 mm, b = 100 mm, and the load mass is 0.5 kg.

In Graph (1), obtain the point at which the vertical line of a = 100 mm and the line of the load shape 5 intersect. Move this intersection point to Graph (2), and the point at which it intersects with the curve of b = 100 mm indicates that the moment of inertia of the 1 kg mass is  $1.7 \times 10^3 \text{ kg} \cdot \text{m}^3$ .

Since the load mass is 0.5 kg, the actual moment of inertia is  $1.7 \times 10^{-3} \times 0.5 = 0.85 \times 10^{-3} \text{ kg} \cdot \text{m}^2$ .





## **2** Calculation of Required Torque

### 2-1 Load Type

The calculation method of required torque varies depending on the load type. Obtain the required torque referring to the table below.

	Load type											
Static load: Ts	Resistance load: Tf	Inertial load: Ta										
When the pressing force is necessary (clamp, etc.)	When friction force or gravity is applied to the rotation direction	When the load with inertia is rotated										
F F	Gravity acts mg mg Friction force acts	The center of rotation and the center of gravity are corresponding  The rotational axis is vertical (up and down)										
Ts = F-L  Ts: Static load (N-m) F: Clamp force (N) L: Distance from the center of rotation to clamp (m)	When gravity acts to the rotation direction  Tf = m·g·L  When friction force acts to the rotation direction  Tf = μ·m·g·L  Tf : Resistance load (N·m)  m : Mass of load (kg)  g : Gravitational acceleration 9.8 (m/s²)  L : Distance from the center of rotation to the gravity or friction force acting point (m)  μ : Coefficient of friction	Ta = I·ώ = I· 2θ t²  Ta: Inertial load (N·m) I: Moment of inertia (kg·m²) ώ: Angular acceleration (rad/s²) θ: Rotating angle (rad) t: Rotation time (s)										
Required torque <b>T</b> = <b>Ts</b>	Required torque <b>T</b> = <b>Tf</b> x (3 to 5) Note 1)	Required torque <b>T</b> = <b>Ta</b> x 10 Note 1)										

Resistance loads → Gravity or friction applies in the rotation direction.
 Example 1) The axis of rotation is in a horizontal (lateral) direction, and the center of rotation and center of gravity of the load are not the same.
 Example 2) The load slips against the floor while rotating.

\*The necessary torque equals the total of the resistance load and inertial load.

T = Tf x (3 to 5) + Ta x 10

Non-resistance loads 
 Gravity or friction does not apply in the rotation direction.
 Example 1) The axis of rotation is in a perpendicular (vertical) direction.
 Example 2) The axis of rotation is in a horizontal (lateral) direction, and the

center of rotation and center of gravity of the load are the same.

\*The necessary torque equals the inertial load only.

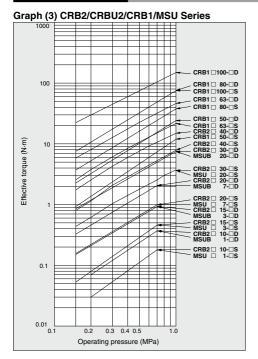
 $T = Ta \times 10$ 

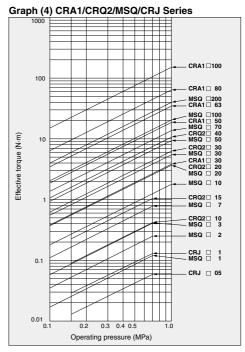
Note 1) In order to adjust the velocity, it is necessary to have a margin of adjustment for Tf and Ta.

⇒P.41 Effective torque ⇒P.41 and 42 Effective torque for each equipment



## **2**-2 Effective Torque





## **2**-3 Effective Torque for Each Equipment

#### Vane Type: CRB2/CRBU2/CRB1 Series







**CRBU2 Series** 



**CRB1 Series** 

S												(N·m)
	Size	Vane type			O	perating	pressu	ıre (MP	a)			
	Size	varie type	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
	10	Single vane	_	0.03	0.06	0.09	0.12	0.15	0.18	_	_	_
	10	Double vane	_	0.07	0.13	0.19	0.25	0.31	0.37	_	_	_
	15	Single vane	0.06	0.10	0.17	0.24	0.32	0.39	0.46	_	_	_
	13	Double vane	0.13	0.20	0.34	0.48	0.65	0.79	0.93	_	_	_
	20	Single vane	0.16	0.23	0.39	0.54	0.70	0.84	0.99	_	_	_
	20	Double vane	0.33	0.47	0.81	1.13	1.45	1.76	2.06	_	_	_
	30	Single vane	0.44	0.62	1.04	1.39	1.83	2.19	2.58	3.03	3.40	3.73
	30	Double vane	0.90	1.26	2.10	2.80	3.70	4.40	5.20	6.09	6.83	7.49
	40	Single vane	0.81	1.21	2.07	2.90	3.73	4.55	5.38	6.20	7.03	7.86
	70	Double vane	1.78	2.58	4.30	5.94	7.59	9.24	10.89	12.5	14.1	15.8
	50	Single vane	1.20	1.86	3.14	4.46	5.69	6.92	8.14	9.5	10.7	11.9
	30	Double vane	2.70	4.02	6.60	9.21	11.8	14.3	16.7	19.4	21.8	24.2
	63	Single vane	2.59	3.77	6.11	8.45	10.8	13.1	15.5	17.8	20.2	22.5
	03	Double vane	5.85	8.28	13.1	17.9	22.7	27.5	32.3	37.10	41.9	46.7
	80	Single vane	4.26	6.18	10.4	14.2	18.0	21.9	25.7	30.0	33.8	37.6
	00	Double vane	8.70	12.6	21.1	28.8	36.5	44.2	51.8	60.4	68.0	75.6
	100	Single vane	8.6	12.2	20.6	28.3	35.9	43.6	51.2	59.7	67.3	75
	100	Double vane	17.9	25.2	42.0	57.3	72.6	87.9	103	120	135	150



## **2**-3 Effective Torque for Each Equipment

#### Vane Type/Rotary Table: MSU Series

(N·m)

MSUA Series	MSUB Series

											(,
Size	Vane type	Operating pressure (MPa)									
Size	varie type	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
1	Single vane	-	0.03	0.06	0.09	0.11	0.14	0.17	-	-	-
	Double vane	-	0.06	0.12	0.18	0.23	0.29	0.35	-	-	-
3	Single vane	0.05	0.09	0.16	0.23	0.31	0.38	0.45	-	-	-
3	Double vane	0.11	0.18	0.32	0.46	0.62	0.77	0.91	-	-	-
7	Single vane	0.14	0.21	0.37	0.52	0.69	0.83	0.98	-	-	-
,	Double vane	0.29	0.44	0.78	1.10	1.42	1.74	2.04	-	-	-
20	Single vane	0.40	0.58	0.99	1.38	1.78	2.19	2.58	2.99	3.39	3.73
20	Double vane	0.86	1.22	2.04	2.82	3.63	4.43	5.22	6.04	6.83	7.49

<sup>\*</sup> Double vane type is MSUB Series only.

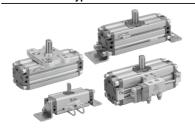
#### Rack & Pinion Type: CRJ Series



							(N·m)				
	Operating pressure (MPa)										
Size	0.15	0.2	0.3	0.4	0.5	0.6	0.7				
05	0.013	0.017	0.026	0.034	0.042	0.050	0.059				
1	0.029	0.038	0.057	0.076	0.095	0.11	0.13				

#### Rack & Pinion Type: CRA1 Series

(N·m)



	Operating pressure (MPa)								
0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
0.38	0.76	1.14	1.53	1.91	2.29	2.67	3.05	3.44	3.82
1.85	3.71	5.57	7.43	9.27	11.2	13.0	14.9	16.7	18.5
3.44	6.88	10.4	13.8	17.2	20.6	24.0	27.5	31.0	34.4
6.34	12.7	19.0	25.3	31.7	38.0	44.4	50.7	57.0	63.4
14.9	29.7	44.6	59.4	74.3	89.1	104	119	133	149
	0.38 1.85 3.44 6.34	0.38 0.76 1.85 3.71 3.44 6.88 6.34 12.7	0.38     0.76     1.14       1.85     3.71     5.57       3.44     6.88     10.4       6.34     12.7     19.0	0.10         0.20         0.30         0.40           0.38         0.76         1.14         1.53           1.85         3.71         5.57         7.43           3.44         6.88         10.4         13.8           6.34         12.7         19.0         25.3	0.10         0.20         0.30         0.40         0.50           0.38         0.76         1.14         1.53         1.91           1.85         3.71         5.57         7.43         9.27           3.44         6.88         10.4         13.8         17.2           6.34         12.7         19.0         25.3         31.7	0.10         0.20         0.30         0.40         0.50         0.60           0.38         0.76         1.14         1.53         1.91         2.29           1.85         3.71         5.57         7.43         9.27         11.2           3.44         6.88         10.4         13.8         17.2         20.6           6.34         12.7         19.0         25.3         31.7         38.0	0.10         0.20         0.30         0.40         0.50         0.60         0.70           0.38         0.76         1.14         1.53         1.91         2.29         2.67           1.85         3.71         5.57         7.43         9.27         11.2         13.0           3.44         6.88         10.4         13.8         17.2         20.6         24.0           6.34         12.7         19.0         25.3         31.7         38.0         44.4	0.10         0.20         0.30         0.40         0.50         0.60         0.70         0.80           0.38         0.76         1.14         1.53         1.91         2.29         2.67         3.05           1.85         3.71         5.57         7.43         9.27         11.2         13.0         14.9           3.44         6.88         10.4         13.8         17.2         20.6         24.0         27.5           6.34         12.7         19.0         25.3         31.7         38.0         44.4         50.7	0.10         0.20         0.30         0.40         0.50         0.60         0.70         0.80         0.90           0.38         0.76         1.14         1.53         1.91         2.29         2.67         3.05         3.44           1.85         3.71         5.57         7.43         9.27         11.2         13.0         14.9         16.7           3.44         6.88         10.4         13.8         17.2         20.6         24.0         27.5         31.0           6.34         12.7         19.0         25.3         31.7         38.0         44.4         50.7         57.0

#### Rack & Pinion Type: CRQ2 Series

(N·m)



		Operating pressure (MPa)									
Size	0.10	0.15	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
10	-	0.09	0.12	0.18	0.24	0.30	0.36	0.42	-	-	
15	-	0.22	0.30	0.45	0.60	0.75	0.90	1.04	-	-	-
20	0.37	0.55	0.73	1.10	1.47	1.84	2.20	2.57	2.93	3.29	3.66
30	0.62	0.94	1.25	1.87	2.49	3.11	3.74	4.37	4.99	5.60	6.24
40	1.06	1.59	2.11	3.18	4.24	5.30	6.36	7.43	8.48	9.54	10.6
	•	•		•		•			•		

#### Rack & Pinion Type/Rotary Table: MSQ Series



										(N·m)
	Operating pressure (MPa)									
Size	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
1	0.017	0.035	0.052	0.070	0.087	0.10	0.12	-	-	-
2	0.035	0.071	0.11	0.14	0.18	0.21	0.25	-	-	-
3	0.058	0.12	0.17	0.23	0.29	0.35	0.41	-	-	-
7	0.11	0.22	0.33	0.45	0.56	0.67	0.78	-	-	-
10	0.18	0.36	0.53	0.71	0.89	1.07	1.25	1.42	1.60	1.78
20	0.37	0.73	1.10	1.47	1.84	2.20	2.57	2.93	3.29	3.66
30	0.55	1.09	1.64	2.18	2.73	3.19	3.82	4.37	4.91	5.45
50	0.93	1.85	2.78	3.71	4.64	5.57	6.50	7.43	8.35	9.28
70	1.36	2.72	4.07	5.43	6.79	8.15	9.50	10.9	12.20	13.6
100	2.03	4.05	6.08	8.11	10.1	12.2	14.2	16.2	18.20	20.3
200	3.96	7.92	11.9	15.8	19.8	23.8	27.7	31.7	35.60	39.6



## **3** Confirmation of Rotation Time

Rotation time adjustment range is specified for each product for stable operation. Set the rotation time within the rotation time specified below.

						Rotati	ion tii	me a	djus	stme	ent range <sup>S</sup> /90°								
Model	0.02	0.03	0.05	0.1	0.2	0.3	0.	.5			1 2	3	4	5			10	20	30
			Si	ze: 10, 15, 20					+							$\top$			
CRB2	i			Size: 30					Ī	П	i i	i	i	Ī	1 1	Ī	<u> </u>	i	i
	i	- !	<u> </u>	Size	e: 40			i	i	ii	<u> </u>	i_	<u> </u>	i	<u>i i</u>	<u> </u>	<u> </u>	i_	
CRB1	-		1 1 1		Size: 5	0, 63, 80	0, 10	0			!	-	-	-	1 1	1	!	- !	- !
	i		Si	ze: 10, 15, 20				i i	i	ш	<u> </u>	<u>i</u>	<u>i</u>	<u>i</u>	<u>i i</u>	<u>i</u>	<u> </u>	<u>i</u>	<u>i</u>
CRBU2		i_	<u> </u>	Size: 30				-	+	11				_	1 1	-	-		
	- 1		<u>i i i</u>		e: 40			_ i	i	<u>i i</u>	i	-	1		1 1	1	!		- !
MSU□	i_	<u>i</u>	1 1 1	Size: 1, 3				-	+	<u> </u>						<u> </u>	<u> </u>		
CRJ	-		<u>i i i</u>		Size: 0			i_	Ī	Ιİ	-	+	1	_	1 1	÷i.	<del>                                     </del>		
	i_		+ + +	<del>                                     </del>		S	ize:		_		<u> </u>	÷	÷	÷	ij	+	<u>i — </u>	<u>i</u> _	_ <u>i</u> _
		_i_	1 1 1	1 1 1		Size: 50 Size: 63						_	+	+	+ +	++	+		
CRA1		-	<del>i i i</del>	<del>                                     </del>		Size: 80								-					
	i_	<del>- i-</del>	+ + +	1 1 1		Size: 100													
		<del></del>	+++	<del>! ! ! !</del>							: 50, 63, 80, 100	(Air b	ıdro	cnoo	ificat	ion)			+
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		- 1	1 1 1					Siz	e: 2	200	•		Ţ		1 1	11	i	i	

<sup>\*:</sup> In case of basic type/with external shock absorber.



If the product is used in a low speed range which is outside the adjustment range, it may cause the stick-slip phenomenon, or the product to stick or stop.

<sup>\*</sup> For the CRA1 series air-hydro type, combine with an air-hydro unit (CC series) and set the rotation time.

# Calculation of Kinetic Energy

Kinetic energy is generated when the load rotates. Kinetic energy applies on the product at the operating end as inertial force, and may cause the product to damage. In order to avoid this, the value of allowable kinetic energy is determined for each product. Find the kinetic energy of the load, and verify that it is within the allowable range for the product in use.

#### Kinetic Energy

Use the following formula to calculate the kinetic energy of the load.

$$\mathbf{E} = \frac{1}{2} \cdot \mathbf{I} \cdot \mathbf{\omega}^2$$

E: Kinetic energy (J)

I: Moment of inertia (kg·m²)

ω: Angle speed (rad/s)

\* For the MSU Series, add the values shown in the table below to the moment of inertia of the load when calculating.

Model	Additional value of moment of inertia; Io
MSU□ 1	2.5 x 10 <sup>-6</sup>
MSU□ 3	6.2 x 10 <sup>−6</sup>
MSU□ 7	1.6 x 10 <sup>-5</sup>
MSU□20	2.8 x 10 <sup>-5</sup>

Kinetic energy formula for MSU series

$$\mathbf{E} = \frac{1}{2} (I + I_0) \omega^2$$

#### Angle Speed

$$\omega = \frac{2\theta}{t}$$

ω: Angle speed (rad/s)

θ: Rotation angle (rad)

t: Rotation time (s)

However, for the air-hydro type, when the rotation time for 90° becomes longer than 2 seconds, use the following formula.

$$\omega = \frac{\theta}{\mathbf{t}}$$

⇒P.45 Allowable kinetic energy and rotation time adjustment range

⇒P.46 to 48 Moment of inertia and rotation time

To find the rotation time when kinetic energy is within the allowable range for the product, use the following formula.

When the rotation angle is  $\omega = \frac{2\theta}{t}$ 

$$t \ge \sqrt{\frac{2 \cdot I \cdot \theta^2}{E}}$$

t: Rotation time (s)

I: Moment of inertia (kg-m2)

θ: Rotation angle (rad)

E: Kinetic energy (J)

When the rotation angle is  $\omega = \frac{\theta}{t}$ 

$$t \! \geq \! \sqrt{\frac{I \! \cdot \! \theta^2}{2 \text{E}}}$$

#### 4-1 Allowable Kinetic Energy and Rotation Time Adjustment Range

#### Table (1a) Allowable Kinetic Energy and Rotation Time Adjustment Range of the Single Vane

	Allowable kine	etic energy (J)	Adjustable range of					
Model	Without	With	rotation time safe in operation					
	rubber bumper	rubber bumper	(S/90°)					
CRB2   10	0.00015	_						
CRB2 □ 15	0.00025	0.001	0.03 to 0.3					
CRB2 □ 20	0.00040	0.003						
CRB2 □ 30	0.015	0.020	0.04 to 0.3					
CRB2 □ 40	0.030	0.040	0.07 to 0.5					
CRB1 □ 50	0.0	0.082						
CRB1 □ 63	0.13	0.120						
CRB1 □ 80	0.3	0.398						
CRB1 □100		0.600						
CRBU2□ 10	0.00015	_						
CRBU2□ 15	0.00025	0.001	0.03 to 0.3					
CRBU2□ 20	0.0004	0.003						
CRBU2□ 30	0.015	0.02	0.04 to 0.3					
CRBU2□ 40	0.030	0.040	0.07 to 0.5					
MSUA 1	0.0065	_						
MSUA 3	0.017	_						
MSUA 7	0.042	_						
MSUA 20	0.073	_	0.074-0.0					
MSUB 1	0.005	_	0.07 to 0.3					
MSUB 3	0.013	_						
MSUB 7	0.032	_						
MSUB 20	0.056	_						

#### Table (1b) Allowable Kinetic Energy and Rotation Time Adjustment Range of the Double Vane

	Allowable kine	etic energy (J)	Adjustable range of		
Model	Without	With	rotation time safe in operation		
	rubber bumper	rubber bumper	(S/90°)		
CRB2   10	0.0003	_			
CRB2 □ 15	0.0005	0.0012	0.03 to 0.3		
CRB2   20	0.0007	0.0033			
CRB2 □ 30	0.015	0.020	0.04 to 0.3		
CRB2 □ 40	0.030	0.040	0.07 to 0.5		
CRB1 □ 50	0.1	12			
CRB1   63	0.1	160	0.44-4		
CRB1 □ 80	0.5	540	0.1 to 1		
CRB1 □100	0.0	0.811			
CRBU2□ 10	0.0003	_			
CRBU2□ 15	0.0005	0.0012	0.03 to 0.3		
CRBU2□ 20	0.0007	0.0033			
CRBU2□ 30	0.015	0.020	0.04 to 0.3		
CRBU2□ 40	0.030	0.040	0.07 to 0.5		
MSUB 1	0.005	_			
MSUB 3	0.013	_	0.074-0.0		
MSUB 7	0.032	_	0.07 to 0.3		
MSHR 20	0.056	_			

Note) Not using rubber bumper means that the rotary actuator is stopped in the middle of its rotation through the use of an external stopper.

Note) Using a rubber bumper means that the rotary actuator is stopped at the representative station and business in the representative station and business in the respective station and business in the respective station and business in the respective station and the respective station and the respective station and the respective station and the respective station and the respective station and the respective station and the rotary actuator is stopped at the respective station and the respective station are respective station.

the respective rotation ends by using an internal stopper.

#### Table (2) Allowable Kinetic Energy and Rotation Time Adjustment Range

	Allowable kine	tic energy (J)	Cushion		le range of	
Model	Without	With	angle	rotation time	safe in operation	
		rubber bumper	angic	(5/	90°) <sup>'</sup>	
CRJ □ 05	0.00025	_		1		
0110 🗆 00	0.001 *1	_	_	0.1	to 0.5	
CRJ □ 1	0.00040	_	_	] 0.1	10 0.5	
	0.002*1	_	_			
CRA1 □ 30	0.010	0.120*2		0.2		
CRA1 □ 50	0.050	0.980 *2		0.2		
CRA1□ 63	0.120	1.500 *2	35°	0.2	to 3	
CRA1 □ 80	0.160	2.000 *2		0.2		
CRA1 □100	0.540	2.900 *2		0.2	to 5	
CRQ2□ 10	0.00025	_		0.2	to 0.7	
CRQ2□ 15	0.00039	_		0.2	10 0.7	
CRQ2□ 20	0.025	0.120 *2				
CRQ2□ 30	0.048	0.250 *2	40°	0.2	to 1	
CRQ2□ 40	0.081	0.400 *2				
MSQ □ 1	0.001	_	_			
MSQ □ 2	0.0015	_		0.2	to 0.7	
MSQ □ 3	0.002	_	_	1		
MSQ □ 7	0.006	_	_	0.2	to 1	
		0.039*3	52°		0.2 to 0.7 × 3	
MSQ □ 10	0.007	0.161*4	7.1°			
		0.231*5	8.6°	0.2 to 1		
		0.116*3	43°		0.2 to 0.7 ×3	
MSQ 🗆 20	0.025	0.574*4	6.9°			
		1.060*5	8.0°	0.2 to 1		
		0.116*3	40°		0.2 to 0.7 × 3	
MSQ □ 30	0.048	0.805*4	6.2°			
		1.210*5	7.3°	0.2 to 1		
		0.294*3	60°		0.2 to 0.7 *3	
MSQ 🗆 50	0.081	1.310*4	9.6°	]		
		1.820*5	10.5°	0.2 to 1		
MSQB 70	0.24	1.100*3	71°	0.2 to 1.5		
MSQB 100	0.32	1.600*3	62°	0.2 to 2	0.2 to 1*3	
MSQB 200	0.56	2.900 *3	82°	0.2 to 2.5	]	

- \*1 Represents external stopper.
- \*2 When the cushion needle with air cushion is adjusted optimally.
- \*3 Represents internal shock absorber.
- \*4 Represents external and low energy type shock absorber.
- \*5 Represents external and high energy type shock absorber.

#### Calculation Example

Load form: Round rod Length of a1 part: 0.12 m Rotation angle: 90° Length of a2 part: 0.04 m Rotation time: 0.9 S/90° Mass of a1 part (= m1): 0.09 kg Mass of a<sub>2</sub> part (= m<sub>2</sub>): 0.03 kg (Step 1) Find the angle speed  $\omega$ = 3.489 rad/s (Step 2) Find the moment of inertia I.  $= \frac{0.09 \times 0.12^2}{3} + \frac{0.03 \times 0.04^2}{3}$  $= 4.48 \times 10^{-4} \text{ kg} \cdot \text{m}^2$ (Step 3) Find the kinetic energy E.  $E = \frac{1}{2} \cdot I \cdot \omega^2 = \frac{1}{2} \times 4.48 \times 10^{-4} \times 3.489^2$ 

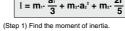
#### Calculation Example

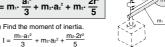
If the model to be used has been determined, obtain the threshold rotation time in which the rotary actuator can be used in accordance with the allowable kinetic energy of that model. : CRA1 = 50 (Without bumper)

Model used

Allowable kinetic energy : 0.05 J (Refer to Table (2)) Load form : Refer to the figure below Rotation angle

 $I = m_{1} \cdot \frac{a_{1}^{2}}{3} + m_{2} \cdot a_{2}^{2} + m_{2} \cdot \frac{2r^{2}}{5}$ 





 $= \frac{0.1 \times 0.12^2}{2} + 0.18 \times 0.15^2 + \frac{0.18 \times 2 \times 0.03^2}{5}$ 

= 4.6 x 10<sup>-3</sup> kg·m<sup>2</sup>

(Step 2) Find the rotating time.

 $t \ge \sqrt{\frac{2 \cdot I \cdot \theta^2}{E}} = \sqrt{\frac{2 \times 4.6 \times 10^{-3} \times (\pi/2)^2}{0.05}} = 0.67s$ 

It is therefore evident that there will be no problem if it is used with a rotation time of less than 0.67s. However, according to table 2, the maximum value of rotation time for stable operation is 2s. Thus, the rotation time should be within the range of 0.67 < t < 2.



a. : 0.12 m a2:0.15 m

m<sub>1</sub>: 0.1 kg

m<sub>2</sub>: 0.18 kg

r : 0.03 m

#### **4**-2 Moment of Inertia and Rotation Time

#### How to read the graph

Example 1) When there are constraints for the moment of inertia of load and rotation time. From "Graph (5)", to operate at the load moment of inertia 1 x 10<sup>-4</sup> kg·m² and at the rotation time setting of 0.3 \$/90°, the models will be

CRB□30-□S and CRB□30-□D.

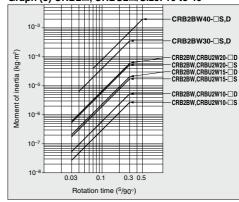
Example 2) When there are constraints for the moment of inertia of load, but not for rotation time. From "Graph (6)", to operate at the load moment of inertia 1 x 10<sup>-2</sup> kg·m<sup>2</sup>:

CRB1 $\square$ 50- $\square$ S will be 0.8 to 1  $^{S}$ /90° CRB1 $\square$ 80- $\square$ S will be 0.35 to 1  $^{S}$ /90° CRB1 $\square$ 100- $\square$ S will be 0.29 to 1  $^{S}$ /90°

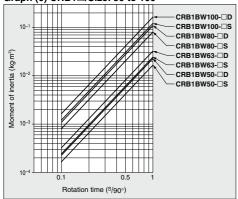
[Remarks] As for the rotation times in "Graphs (5) to (15)", the lines in the graph indicate the adjustable speed ranges. If the speed is adjusted towards the low-speed end beyond the range of the line, it could cause the actuator to stick, or, in the case of the vane type, it could stop its operation.

#### <Vane type: CRB2/CRBU2/CRB1/MSU Series>

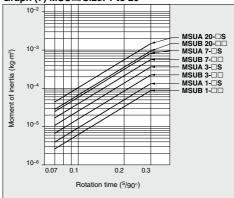
#### Graph (5) CRB2□, CRBU2□/Size: 10 to 40



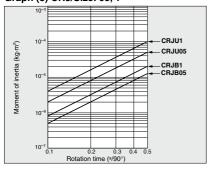
#### Graph (6) CRB1□/Size: 50 to 100



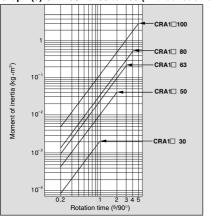
#### Graph (7) MSU□/Size: 1 to 20



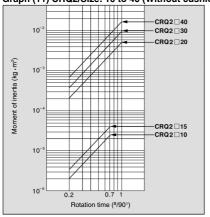
<Rack & pinion type: CRJ/CRA1 Series> Graph (8) CRJ/Size: 05, 1



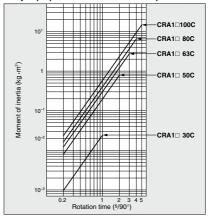
Graph (9) CRA1/Size: 30 to 100 (Without cushion)

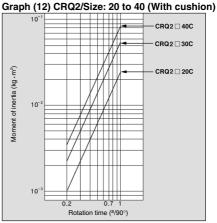


<Rack & pinion type: CRQ2/MSQ Series> Graph (11) CRQ2/Size: 10 to 40 (Without cushion)



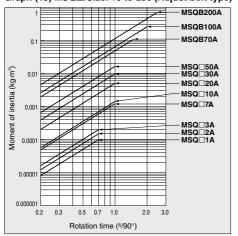
Graph (10) CRA1/Size: 30 to 100 (With cushion)



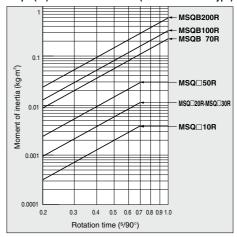


#### **4-2** Moment of Inertia and Rotation Time

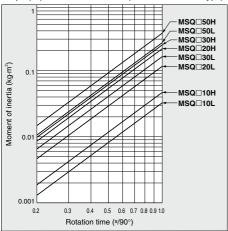
Graph (13) MSQ□/Size: 10 to 200 (Adjust bolt type)



Graph (14) MSQ□/Size: 10 to 200 (Internal absorber type)

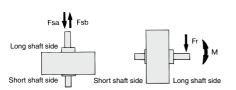


Graph (15) MSQ□/Size: 10 to 50 (External absorber type)



## **6** Confirmation of Allowable Load

Provided that a dynamic load is not generated, a load in the axial direction can be applied up to the value that is indicated in the table below. However, applications in which the load is applied directly to the shaft should be avoided as much as possible.









#### Vane Type

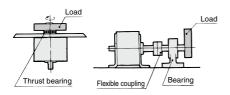
### Vane Type (Single, Double)

Series	Model		Load direction							
Jenes	Wodei	Fsa (N)	Fsb (N)	Fr (N)	M (N·m)					
	CRB2 🗆 10	9.8	9.8	14.7	0.13					
	CRB2 🗆 15	9.8	9.8	14.7	0.17					
	CRB2 🗆 20	19.6	19.6	24.5	0.33					
	CRB2   30	24.5	24.5	29.4	0.42					
CRB2	CRB2   40	40	40	60	1.02					
	CRB1 🗆 50	196	196	245	8.09					
	CRB1   63	340	340	390	14.04					
	CRB1   80	490	490	490	20.09					
	CRB1 □100	539	539	588	30.28					
	CRBU2□ 10	9.8	9.8	14.7	0.13					
	CRBU2□ 15	9.8	9.8	14.7	0.17					
CRBU2	CRBU2□ 20	19.6	19.6	24.5	0.33					
	CRBU2□ 30	24.5	24.5	29.4	0.42					
	CRBU2□ 40	40	40	60	1.02					

#### Vane Type (Single, Double)

Series	Model	Load direction							
Series	iviodei	Fsa (N)	Fsb (N)	Fr (N)	M (N·m)				
	MSUA 1	15	15	20	0.3				
MSUA	MSUA 3	30	30	40	0.7				
WISUA	MSUA 7	60	60	50	0.9				
	MSUA20	80	80	60	2.9				
	MSUB 1	10	15	20	0.3				
MSUB	MSUB 3	15	30	40	0.7				
	MSUB 7	30	60	50	0.9				
	MSUB20	40	80	60	2.9				

Provided that a dynamic load is not generated, a load that is within the allowable radial/thrust load can be applied. However, applications in which the load is applied directly to the shaft should be avoided as much as possible. The methods such as those described below are recommended to prevent the load from being applied directly to the shaft in order to ensure a proper operating condition.



#### Rack & Pinion Type

#### Rack & Pinion Type (Single rack)

Series	Mandal	Load direction							
Series	Model	Fsa (N)	Fsb (N)	Fr (N)	M (N·m)				
CRJ	CRJ□ 05	20	20	25	0.26				
CHJ	CRJ□ 1	25	25	30	0.32				

#### Rack & Pinion Type (Single rack)

Series	Model	Load direction							
Selles	iviodei	Fsa (N)	Fsb (N)	Fr (N)	M (N·m)				
	CRA1□ 30	29.4	29.4	29.4	0.44				
	CRA1□ 50	490	196	196	3.63				
CRA1	CRA1□ 63	588	196	294	6.17				
	CRA1□ 80	882	196	392	9.80				
	CRA1□100	980	196	588	19.11				

#### Rack & Pinion Type (Double rack)

Series	Model	Load direction								
Series	iviouei	Fsa (N)	Fsb (N)	Fr (N)	M (N·m)					
	CRQ2B□10	15.7	7.8	14.7	0.21					
	CRQ2B□15	19.6	9.8	19.6	0.32					
CRQ2	CRQ2B□20	49	29.4	49	0.96					
	CRQ2B□30	98	49	78	1.60					
	CRQ2B□40	108	59	98	2.01					

#### Rack & Pinion Type (Double rack)

			Load di	rection	
Series	Model	Fsa (N)	Fsb (N)	Fr (N)	M (N·m)
	MSQA 1□	41	41	31	0.84
	MSQA 2□	45	45	32	1.2
	MSQA 3□	48	48	33	1.6
MSQA	MSQA 7□	71	71	54	2.2
	MSQA 10□	107	74	86	2.9
	MSQA 20□	197	137	166	4.8
	MSQA 30□	398	197	233	6.4
	MSQA 50□	517	296	378	12.0
	MSQB 1□	41	41	31	0.56
	MSQB 2□	45	45	32	0.82
	MSQB 3□	48	48	33	1.1
	MSQB 7□	71	71	54	1.5
	MSQB 10□	78	74	78	2.4
MSQB	MSQB 20□	137	137	147	4.0
	MSQB 30□	363	197	196	5.3
	MSQB 50□	451	296	314	9.7
	MSQB 70□	476	296	333	12.0
	MSQB100□	708	493	390	18.0
	MSQB200□	1009	740	543	25.0

# **6** Calculation of Air Consumption and Required Air Flow Capacity

Air consumption is the volume of air which is expended by the rotary actuator's reciprocal operation inside the actuator and in the piping between the actuator and the switching valve, etc. This is necessary for selection of a compressor and for calculation of its running cost. Required air volume is the air volume necessary to make a rotary actuator operate at a required speed. It requires calculation when selecting the upstream piping diameter from the switching valve and air line equipment.

\* To facilitate your calculation, Tables (1) to (5) provide the air consumption volume (QcR) that is required each time an individual rotary actuator makes a reciprocal movement.

#### 1. Air consumption volume

#### Formula

Regarding QCR: With vane type sizes 10 to 40, use formula (1) because the internal volume varies when ports A and B are pressurized. For vane type sizes 50 to 100, as well as for the rack and pinion type, use formula (2).

$$Q_{CR} = (V_A + V_B) \times \left(\frac{P + 0.1}{0.1}\right) \times 10^{-3}$$

$$Q_{CR} = 2 \times V_A \times \left(\frac{P + 0.1}{0.1}\right) \times 10^{-3}$$

$$Q_{CP} = 2 \times a \times L \times \left(\frac{P}{0.1}\right) \times 10^{-8}$$

$$Q_{CR} = Q_{CR} + Q_{CP}$$

$$(3)$$

$$Q_{CR} = Q_{CR} + Q_{CR}$$

$$(4)$$

Qca = Amount of air consumption of rotary actuator 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Inner volume of the rotary actuator (when pressurized from A port) 
Qca = Amount of air consumption of tube or piping 
Qca = Inner volume of the rotary actuator (when pressurized from B port) 
Qca = Amount of air consumption Qca = Inner volume of the rotary actuator (when pressurized from B port) 
Qca = Amount of air consumption Qca = Inner volume of the rotary actuator (when pressurized from B port) 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
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Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of tube or piping 
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Qca = Amount of air consumption of tube or piping 
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Qca = Amount of air consumption of tube or piping 
Qca = Amount of air consumption of air consumption of air consumption of air consumption of air consumption of air consumption of air consumption of air consumption of air consumption of air consumption of

Qc = Amount of air consumption required for one cycle of the rotary actuator [L(ANR)]

To select a compressor, it is important to select one that has plenty of margin to accommodate the total air volume that is consumed by the pneumatic actuators that are located downstream. The total air consumption volume is affected by the leakage in the tube, the consumption in the drain valves and pilot valves, as well as by the reduction in air volume due to reduced temperature.

#### Formula

$Q_{c2} = Q_c \times n \times No.$ of actuators x Space rate(5)
---

 $Qc_2 = Amount of air from a compressor$ 

n = Actuator reciprocations per minute

Safety factor: from 1.5

#### 2. Required air flow capacity

#### Formula

Or: Make use of formulas (6) and (7) for the vane type, and double the results of formula (7) for the rack and pinion type.

$$\begin{split} Q_r &= \left\{ V_B \ x \left( \frac{P}{0.1} + 0.1 \right) x \ 10^{-3} + a \ x \ L \ x \left( \frac{P}{0.1} \right) x \ 10^{-6} \right\} \ x \ \frac{60}{t} \cdots \cdots (6) \\ Q_r &= \left\{ V_A \ x \left( \frac{P}{0.1} \right) x \ 10^{-3} + a \ x \ L \ x \left( \frac{P}{0.1} \right) x \ 10^{-6} \right\} \ x \ \frac{60}{t} \cdots \cdots (7) \end{split}$$

Qr=Consumed air volume for rotary actuator [L/r

V<sub>A</sub> = Inner volume of the rotary actuator (when pressurized from A port)

V<sub>B</sub> = Inner volume of the rotary actuator (when pressurized from B port) [cm<sup>3</sup>]

P = Operating pressure [MPa]
L = Length of piping [mm]

[cm<sup>3</sup>]

a = Inner sectional area of piping [mm²]

t=Total time for rotation [S]

#### Internal Cross Section of Tubing and Steel Piping

			<u> </u>
Nominal	O.D. (mm)	I.D. (mm)	Internal cross section a (mm²)
T□ 0425	4	2.5	4.9
T□ 0604	6	4	12.6
TU 0805	8	5	19.6
T□ 0806	8	6	28.3
1/8B	_	6.5	33.2
T□ 1075	10	7.5	44.2
TU 1208	12	8	50.3
T□ 1209	12	9	63.6
1/4B	_	9.2	66.5
TS 1612	16	12	113
3/8B	_	12.7	127
T□ 1613	16	13	133
1/2B	_	16.1	204
3/4B	_	21.6	366
1B	_	27.6	598

<sup>⇒</sup>P.51 and 52 Inner volume and air consumption

[L/min (ANR)]

<sup>⇒</sup>P.53 and 54 Air consumption calculation graph

## **1** Inner Volume and Air Consumption

Vane	0:	Rotation	Inner volu	ime (cm³)	Operating pressure (MPa)									
vane	Size	(degree)	Press. V <sub>A</sub> port	Press. V <sub>B</sub> port	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
		90	0.6	1.0	_	0.005	0.006	0.008	0.010	0.011	0.013	_	_	_
	10	180	1.2	1.2	_	0.007	0.010	0.012	0.014	0.017	0.019	_	_	_
		270	1.5	1.5	_	0.009	0.012	0.015	0.018	0.021	0.024	_	_	_
		90	1.0	1.5	0.006	0.008	0.010	0.013	0.015	0.018	0.020	_	_	_
	15	180	2.9	2.9	0.015	0.017	0.023	0.029	0.035	0.041	0.046	_	_	_
		270	3.7	3.7	0.019	0.022	0.030	0.037	0.044	0.052	0.059	_	_	_
		90	3.6	4.8	0.021	0.025	0.034	0.042	0.050	0.059	0.067			_
	20	180	6.1	6.1	0.031	0.037	0.049	0.061	0.073	0.085	0.098			_
		270	7.9	7.9	0.040	0.047	0.063	0.079	0.095	0.111	0.126			_
		90	8.5	11.3	0.050	0.059	0.079	0.099	0.119	0.139	0.158	0.178	0.198	0.21
	30	180	15	15	0.075	0.090	0.120	0.150	0.180	0.210	0.240	0.270	0.300	0.33
		270	20.2	20.2	0.101	0.121	0.162	0.202	0.242	0.283	0.323	0.364	0.404	0.44
		90	21	25	0.115	0.138	0.184	0.230	0.276	0.322	0.368	0.414	0.460	0.50
	40	180	31.5	31.5	0.158	0.189	0.252	0.315	0.378	0.441	0.504	0.567	0.630	0.693
-		270	41	41	0.205	0.246	0.328	0.410	0.492	0.574	0.656	0.738	0.820	0.90
		90	30	30	0.150	0.180	0.240	0.300	0.360	0.420	0.480	0.540	0.600	0.66
		100	32	32	0.160	0.192	0.256	0.320	0.384	0.448	0.512	0.576	0.640	0.70
Single vane	50	180	49	49	0.245	0.294	0.392	0.490	0.588	0.686	0.784	0.882	0.980	1.078
3		190	51	51	0.255	0.306	0.408 0.528	0.510	0.612	0.714	0.816 1.056	0.918	1.020	1.12
		270	66	66			0.528			0.924		1.188	1.320	1.452
-		280	68	68	0.340	0.408		0.680	0.816	0.952	1.088			1.49
		90	70	70	0.350	0.420	0.560 0.584	0.700	0.840	1.022	1.120	1.260	1.400	1.54
		100	73	73	0.365	0.436	0.564	0.730	1.128	1.316	1.504	1.692	1.880	2.06
	63	180	94	94 97	0.470	0.582	0.752	0.940	1.164	1.358	1.552	1.746	1.940	2.13
		190 270	97 118	118	0.590	0.708	0.776	1.180	1.416	1.652	1.888	2.124	2.360	2.59
		280	121	121	0.605	0.706	0.968	1.210	1.452	1.694	1.936	2.178	2.420	2.66
F		90	88	88	0.440	0.528	0.704	0.880	1.056	1.232	1.408	1.584	1.760	1.936
		100	93	93	0.465	0.558	0.744	0.930	1.116	1.302	1.488	1.674	1.860	2.04
		180	138	138	0.690	0.828	1.104	1.380	1.656	1.932	2.208	2.484	2.760	3.03
	80	190	143	143	0.715	0.858	1.144	1.430	1.716	2.002	2.288	2.574	2.860	3.14
		270	188	188	0.940	1.128	1.504	1.880	2.256	2.632	3.008	3.384	3.760	4.136
		280	193	193	0.965	1.158	1.544	1.930	2.316	2.702	3.088	3.474	3.860	4.246
F		90	186	186	0.930	1.116	1.488	1.860	2.232	2.604	2.976	3.348	3.720	4.092
		100	197	197	0.985	1.182	1.576	1.970	2.364	2.758	3.152	3.546	3.940	4.33
		180	281	281	1.405	1.686	2.248	2.810	3.372	3.934	4.496	5.058	5.620	6.182
	100	190	292	292	1.460	1.752	2.336	2.920	3.504	4.088	4.672	5.256	5.840	6.42
		270	376	376	1.880	2.256	3.008	3.760	4.512	5.264	6.016	6.768	7.520	8.272
		280	387	387	1.935	2.322	3.096	3.870	4.644	5.418	6.192	6.966	7.740	8.51
		90	1.0	1.0	_	0.006	0.008	0.010	0.012	0.014	0.016	_	_	_
	10	100	1.1	1.1	_	0.007	0.009	0.011	0.013	0.015	0.018	_	_	_
		90	2.6	2.6	0.013	0.016	0.021	0.026	0.031	0.036	0.042	_	_	_
	15	100	2.7	2.7	0.014	0.016	0.022	0.027	0.032	0.038	0.043	_	_	_
	20	90	5.6	5.6	0.028	0.034	0.045	0.056	0.067	0.078	0.090	_	_	_
	20	100	5.7	5.7	0.029	0.034	0.046	0.057	0.068	0.080	0.091	_	_	_
		90	14.4	14.4	0.072	0.086	0.115	0.144	0.173	0.202	0.230	0.259	0.288	0.31
	30	100	14.5	14.5	0.073	0.087	0.116	0.145	0.174	0.203	0.232	0.261	0.290	0.31
		90	33	33	0.165	0.198	0.264	0.330	0.396	0.462	0.528	0.594	0.660	0.72
ouble vane	40	100	34	34	0.170	0.204	0.272	0.340	0.408	0.476	0.544	0.612	0.680	0.74
Jouble vaile		90	48	48	0.240	0.288	0.384	0.480	0.576	0.672	0.768	0.864	0.960	1.05
	50	100	52	52	0.260	0.312	0.416	0.520	0.624	0.728	0.832	0.936	1.040	1.14
		90	98	98	0.490	0.588	0.784	0.980	1.176	1.372	1.568	1.764	1.960	2.15
	63	100	104	104	0.520	0.624	0.832	1.040	1.248	1.456	1.664	1.872	2.080	2.28
		90	136	136	0.680	0.816	1.088	1.360	1.632	1.904	2.176	2.448	2.720	2.99
	80	100	146	146	0.730	0.876	1.168	1.460	1.752	2.044	2.336	2.628	2.920	3.212
		90	272	272	1.360	1.632	2.176	2.720	3.264	3.808	4.352	4.896	5.440	5.98
	100	100	294	294	1.470	1.764	2.352	2.940	3.528	4.116	4.704	5.292	5.880	6.46

Table (2) Vane	Type Rotary	Table: MSU	Series
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Table (2)	vane ryp	e Rotary	rable: MSC	J Series									(	L(ANR))	
Vane	Size	Rotation	Inner volu	ıme (cm³)	Operating pressure (MPa)										
varie	Size	(degree)	Press. V <sub>A</sub> port	Press. V <sub>B</sub> port	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	
	4	90	0.8	1.3	_	0.006	0.008	0.011	0.013	0.015	0.017	_	_	_	
Single vane		180	1.3	1.3	_	0.008	0.010	0.013	0.016	0.018	0.021	_		_	
	,	90	1.9	3.1	0.013	0.015	0.020	0.025	0.030	0.035	0.040	_	_	_	
	3	180	3.1	3.1	0.016	0.019	0.025	0.031	0.037	0.043	0.050	_	_	_	
	7	90	4.0	6.6	0.027	0.032	0.042	0.053	0.064	0.074	0.085		_	_	
	′ [	180	6.6	6.6	0.033	0.040	0.053	0.066	0.079	0.092	0.106	_	_	_	
	20	90	10.1	16.8	0.067	0.081	0.108	0.135	0.161	0.188	0.215	0.242	0.269	0.296	
	20	180	16.8	16.8	0.084	0.101	0.134	0.168	0.202	0.235	0.269	0.302	0.336	0.370	
Davida	1	90	1.1	1.1	_	0.007	0.009	0.011	0.013	0.015	0.018	_	_	_	
Double	3	90	2.7	2.7	0.014	0.016	0.022	0.027	0.032	0.038	0.043	_	_	_	
vane (MSUB only)	7	90	5.7	5.7	0.029	0.034	0.046	0.057	0.068	0.080	0.091	_	_	_	
(IVIOUD UTILY)	20	90	14.5	14.5	0.073	0.087	0.116	0.145	0.174	0.203	0.232	0.261	0.290	0.319	

## **1** Inner Volume and Air Consumption

Table (3) Rack & Pinion Type: CRJ Series											
Size	Rotation (degree)	Volume V <sub>A</sub> (cm <sup>3</sup> )			Opera	ating pressure (	(MPa)				
Size	notation (degree)	Volume VA (Citi)	0.15	0.2	0.3	0.4	0.5	0.6	0.7		
05	90	0.15	0.00074	0.00089	0.0012	0.0015	0.0018	0.0021	0.0024		
03	180	0.31	0.0015	0.0018	0.0025	0.0031	0.0037	0.0043	0.0049		
1	90	0.33	0.0016	0.0020	0.0026	0.0033	0.0039	0.0046	0.0052		
·	180	0.66	0.0033	0.0039	0.0052	0.0065	0.0078	0.0091	0.010		

Table (4)	Rack &	Pinion 1	Type: (	CRA1	Series
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(L	Δ	N	B,	ľ

Size	Detetion (degree)	Volume V <sub>A</sub> (cm <sup>3</sup> )				Ol	perating pr	essure (Mi	Pa)			
Size	Hotation (degree)	volume VA (Cm²)	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
30	90	7.4	0.030	0.044	0.059	0.074	0.089	0.104	0.118	0.133	0.148	0.163
30	180	14	0.056	0.084	0.112	0.140	0.168	0.196	0.224	0.252	0.280	0.308
	90	32	0.128	0.192	0.256	0.320	0.384	0.448	0.512	0.576	0.640	0.704
50	100	36	0.144	0.216	0.288	0.360	0.432	0.504	0.576	0.648	0.720	0.792
50	180	65	0.260	0.390	0.520	0.650	0.780	0.910	1.040	1.170	1.300	1.430
	190	68	0.272	0.408	0.544	0.680	0.816	0.952	1.088	1.224	1.360	1.496
	90	60	0.240	0.360	0.480	0.600	0.720	0.840	0.960	1.080	1.200	1.320
63	100	67	0.268	0.402	0.536	0.670	0.804	0.938	1.072	1.206	1.340	1.474
03	180	120	0.480	0.720	0.960	1.200	1.440	1.680	1.920	2.160	2.400	2.640
	190	127	0.508	0.762	1.016	1.270	1.524	1.778	2.032	2.286	2.540	2.794
	90	111	0.444	0.666	0.888	1.110	1.332	1.554	1.776	1.998	2.220	2.442
80	100	123	0.492	0.738	0.984	1.230	1.476	1.722	1.968	2.214	2.460	2.706
80	180	221	0.884	1.326	1.768	2.210	2.652	3.094	3.536	3.978	4.420	4.862
	190	233	0.932	1.398	1.864	2.330	2.796	3.262	3.728	4.194	4.660	5.126
	90	259	1.036	1.554	2.072	2.590	3.108	3.626	4.144	4.662	5.180	5.698
100	100	288	1.152	1.728	2.304	2.880	3.456	4.032	4.608	5.184	5.760	6.336
100	180	518	2.072	3.108	4.144	5.180	6.216	7.252	8.288	9.324	10.36	11.396
	190	547	2.188	3.282	4.376	5.470	6.564	7.658	8.752	9.846	10.940	12.034

#### Table (5) Rack & Pinion Type: CRQ2 Series

(L(ANR	)
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Size	Rotation (degree)		Operating pressure (MPa)										
			0.1	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
10	90	1.2	_	0.006	0.007	0.009	0.012	0.014	0.016	0.018	_	_	_
	180	2.2		0.011	0.013	0.018	0.022	0.026	0.031	0.035		_	_
	360	4.3	_	0.021	0.026	0.034	0.043	0.051	0.060	0.068	_	_	_
15	90	2.9		0.015	0.017	0.023	0.029	0.035	0.041	0.046	_	_	_
	180	5.5	-	0.028	0.033	0.044	0.055	0.066	0.077	0.088	_	_	_
	360	10.7	_	0.023	0.064	0.086	0.107	0.129	0.193	0.172	_	_	_
20	90	7.1	0.028	0.036	0.043	0.057	0.071	0.085	0.099	0.114	0.128	0.142	0.156
	180	13.5	0.054	0.068	0.081	0.108	0.135	0.162	0.189	0.216	0.243	0.270	0.297
	360	26.3	0.105	0.131	0.158	0.210	0.263	0.316	0.368	0.421	0.473	0.526	0.578
30	90	12.1	0.048	0.060	0.073	0.097	0.121	0.145	0.169	0.193	0.218	0.242	0.266
	180	23.0	0.092	0.115	0.138	0.184	0.230	0.276	0.322	0.368	0.413	0.459	0.505
	360	44.7	0.179	0.224	0.268	0.358	0.447	0.537	0.626	0.716	0.805	0.895	0.984
40	90	20.6	0.082	0.103	0.123	0.164	0.206	0.247	0.288	0.329	0.370	0.411	0.452
	180	39.1	0.156	0.195	0.234	0.313	0.391	0.469	0.547	0.625	0.703	0.781	0.859
	360	76.1	0.304	0.380	0.456	0.609	0.761	0.913	1.07	1.22	1.37	1.52	1.67

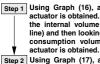
Table (6) Rack & Pinion Type/Rotary Table: MSQ Series

(L(ANR))

Size	(degree)	Volume	Operating pressure (MPa)									
Size		V <sub>A</sub> (cm <sup>3</sup> )	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
1		0.66	0.0026	0.0039	0.0052	0.0065	0.0078	0.0091	0.010	_	_	_
2		1.3	0.0052	0.0077	0.010	0.013	0.015	0.018	0.021	_	_	_
3		2.2	0.0087	0.013	0.017	0.022	0.026	0.030	0.035	_	_	_
7		4.2	0.017	0.025	0.033	0.042	0.050	0.058	0.066	_	_	_
10		6.6	0.026	0.040	0.053	0.066	0.079	0.092	0.106	0.119	0.132	0.145
20	190°	13.5	0.054	0.081	0.108	0.135	0.162	0.189	0.216	0.243	0.270	0.297
30		20.1	0.080	0.121	0.161	0.201	0.241	0.281	0.322	0.362	0.402	0.442
50		34.1	0.136	0.205	0.273	0.341	0.409	0.477	0.546	0.614	0.682	0.750
70		50.0	0.200	0.300	0.400	0.500	0.600	0.700	0.800	0.900	1.000	1.100
100		74.7	0.299	0.448	0.598	0.747	0.896	1.046	1.195	1.345	1.494	1.643
200		145.9	0.584	0.875	1.167	1.459	1.751	2.043	2.334	2.626	2.918	3.210



#### 3-2 Air Consumption Calculation Graph



Step 1 Using Graph (16), air consumption volume of the rotary actuator is obtained. From the point of intersection between the internal volume and the operating pressure (slanted line) and then looking to the side (left side) direction, the air consumption volume for 1 cycle operation of a rotary

Step 2 Using Graph (17), air consumption volume of tubing or steel piping is obtainted.

- (1) First determine the point of intersection between the operating pressure (slanted line) and the piping length, and then go up the vertical line perpendicularly from there. (2) From the point of intersection of an operating piping tube diameter (slanted line), then look to the side (left or right) to obtain the required air consumption volume for piping.
- Step 3 Total air consumption volume per minute is obtained as follows: (Air consumption volume of a rotary actuator [unit: L (ANR)] + Tubing or steel piping's air consumption volume) x Cycle times per minute x Number of rotary actuators = Total air consumption volume
- Example) What is the air consumption volume for 10 units of a CRQ2BS40-90 to actuate by operating pressure 0.5 MPa for one minute .. ? (Distance between actuator and switching valve is the internal diameter 6 mm tubing with 2 m piping.)
  - 1. Operating pressure 0.5 MPa → Internal volume of CRQ2BS40-90 40 cm<sup>3</sup> → Air consumption volume 0.23 L (ANR)
  - 2. Operating pressure 0.5 MPa  $\rightarrow$  Piping length 2 m  $\rightarrow$  Internal diameter 6 mm → Air consumption volume 0.56 L (ANR)
  - 3. Total air consumption volume = (0.23 + 0.56) x 5 x 10 = 39.5 L/min (ANR)

#### Inner Volume: Rack & Pinion Type

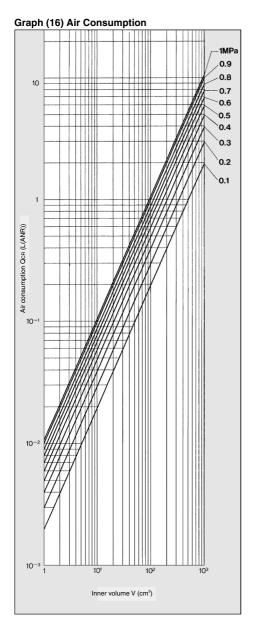
1 cycle (cm<sup>3</sup>)

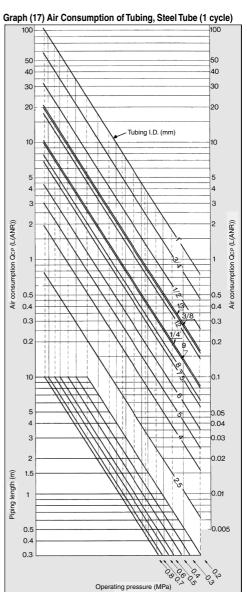
Model	Rotation angle								
Model	90°	100°	180°	190°	360°				
CRJ □ 05	0.3	0.34	0.62	0.66	_				
CRJ □ 1	0.66	0.74	1.32	1.4	_				
CRA1□ 30	14.8	_	28	_	_				
CRA1□ 50	64	72	130	136	_				
CRA1□ 63	120	134	240	254	_				
CRA1□ 80	222	246	442	466	_				
CRA1□100	518	576	1040	1090	_				
CRQ2□ 10	2.4	_	4.4	_	8.6				
CRQ2□ 15	3.8	_	11	_	21.4				
CRQ2□ 20	14.2	_	27	_	52.6				
CRQ2□ 30	24.2	_	46	_	89.4				
CRQ2□ 40	41.2	_	78.2	_	152				
MSQ □ 1	_	_	_	1.3	_				
MSQ □ 2	_	_	_	2.7	_				
MSQ 🗆 3	_	_	_	4.4	_				
MSQ □ 7	_	_	_	8.4	_				
MSQ □ 10	_	_	_	13.1					
MSQ □ 20	_	_	_	27.0	_				
MSQ □ 30	_	_	_	40.2					
MSQ □ 50	_	_	_	68.4	_				
MSQB 70	_	_	_	100					
MSQB 100	_	_	_	149	_				
MSQB 200	_	_	_	292	_				

Inner Volume: Vane Type 1 cycle (cm <sup>3</sup> )									
Model	Rotation angle								
Model	90°	100°	180°	190°	270°	280°			
CRB □ 10-□S	1.6	_	2.4	_	3	_			
CRB □ 15-□S	2.5	_	5.8	_	7.4	_			
CRB □ 20-□S	8.4	_	12.2	-	15.8	_			
CRB □ 30-□S	19.8	_	30	_	40	_			
CRB □ 40-□S	25	_	31.5	_	41				
CRB1□ 50-□S	60	64	98	102	132	136			
CRB1□ 63-□S	70	73	94	97	118	121			
CRB1□ 80-□S	176	186	276	286	376	386			
CRB1□100-□S	372	394	562	584	752	774			
MSU 1-□S	2.1	_	2.6	_	_	_			
MSU 3-□S	5.0	_	6.2	_	_				
MSU 7-□S	10.6	_	13.2	_	_	_			
MSU 20-□S	26.9	_	33.6	_	_				
CRB 10-□D	2	2.2	_	_	_	_			
CRB 15-□D	5.2	5.4	_	_	_				
CRB 20-□D	11.2	11.4	_	_	_	_			
CRB 30-□D	28.8	29	_	_	_				
CRB 40-□D	33	34	_	_	_	_			
CRB1□ 50-□D	96	104	_	_	_				
CRB1□ 63-□D	98	104	_	_	_				
CRB1□ 80-□D	272	292	_	_	_				
CRB1□100-□D	544	588	_	_	_				
MSUB 1-□D	2.2	_	_	_	_				
MSUB 3-□D	5.4	_	_	_	_	_			
MSUB 7-□D	11.4	_		_	_				
MSUB 20-□D	29.0	_	_	_	_	_			



## **3**-2 Air Consumption Calculation Graph





<sup>&</sup>quot;Piping length" indicates length of steel tube or tubing which connects

rotary actuator and switching valves (solenoid valves, etc.).

\* Refer to page 50 for size of tubing and steel tube (inner dimension and outer dimension).

